



FireFOAM to Model inside Battery Thermal Disorder Propagation

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10th FM Global Open Source CFD Fire Modeling Workshop , Norwood MA on May 30 - 31, 2018.



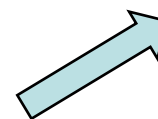
maîtriser le risque |
pour un développement durable |

Energy storage is becoming a critical issue

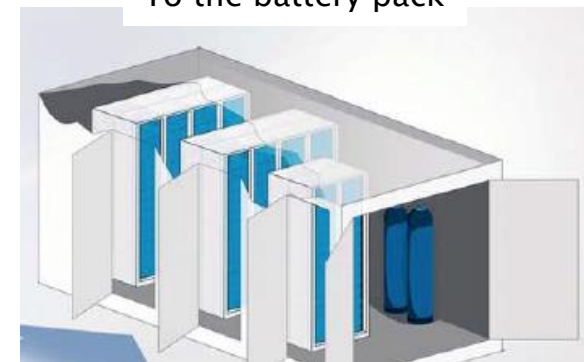
- For stationary applications (renewable generation plants, electric grids, ...)
- For various mobile applications (cars, electronic devices, ...)
- Current Lithium Ion Batteries (LIBs) are more & more used

For all cases, autonomy is a key

- Energy density is increasing → compacity increases
- Battery size is more and more important
- Safety is still highly important



To the battery pack



From the individual cells

Through the module

Safety is commonly addressed using experiments

- Individual cell behavior depending on the chemistry
 - Crash, stability, impact, overcharge, ...
 - Gas production, HRR and other measurements
- Lots of data are available regarding battery testing

The current very large batteries require an innovative approach

- With very large experimental facilities ... up to a certain limit (20 MW in INERIS)
- Using numerical modelling



Several steps to be modelled

1. Ignition in one cell

- Several complex physical phenomena
- Depending on the ignition source (internal short-circuit, overcharge, ...)

2. Gas release and ignition

- Mixture of several flammable gases (EC / DMC / ...)

3. Temperature rise in the surrounding

- Combustion of the emitted gases
- Strong interaction with the air flow and battery structure opening

4. Other cells runaway

- Assuming other cells will be ignited by thermal runaway
- Evaluation of the internal temperature

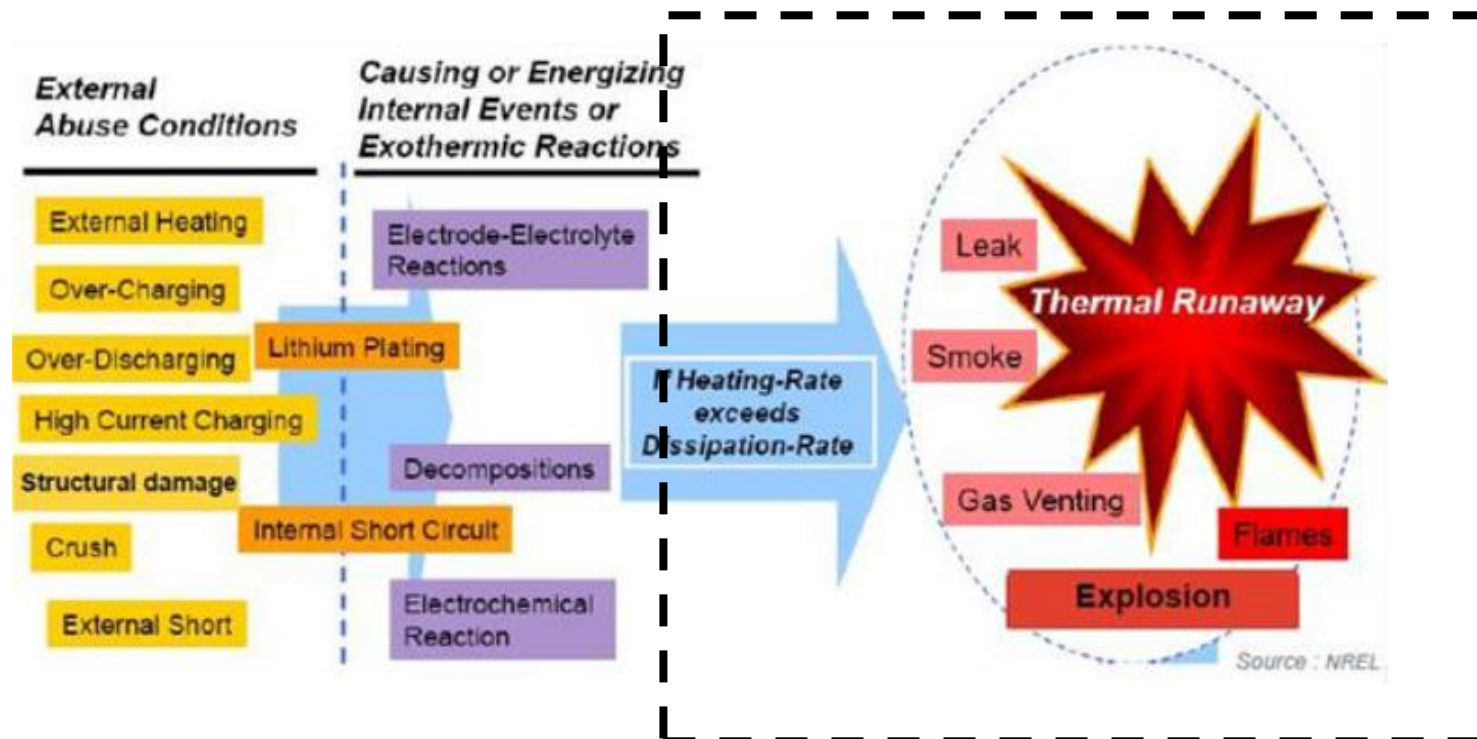
5. Neighbor cells burning

- Similar to the initial burning cell

Ignition of a LIB cell

As usual, ignition is very complex

- Cell ignition depends on the source
 - Short-circuit, overcharging, structural damages, ...
 - Clearly impossible to consider each kind of possible sources
- Hopefully, during the propagation process
 - Ignition mechanism is based on thermal effect



Ignition is a phenomenon governed by inner cell behavior

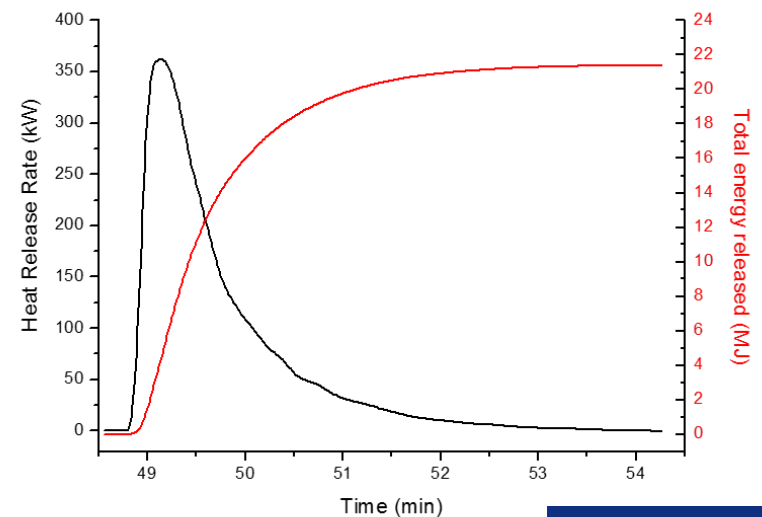
→ We decided not to model phenomena inside the cell

Ignition is considered to occur at a given time

- The HRR from the first cell is fixed thanks to experimental data

This requires

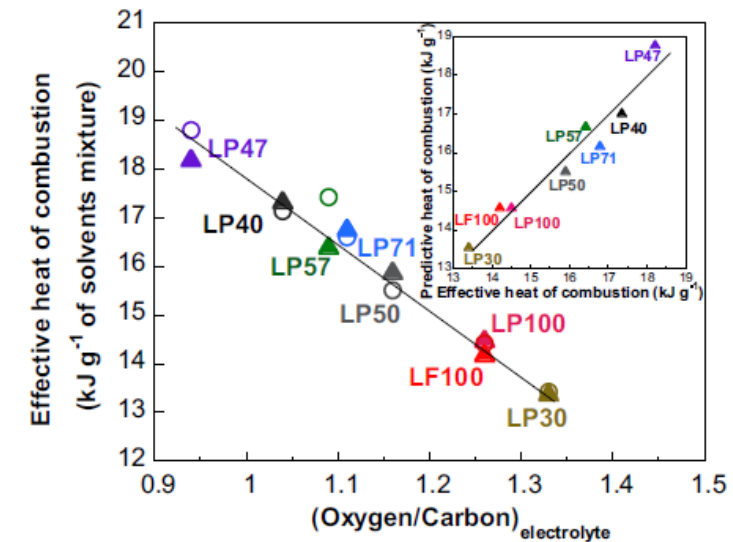
- An experiment at cell scale with HRR measurement
- An experimental control of the failure mode



With the key issue of chemical reactions

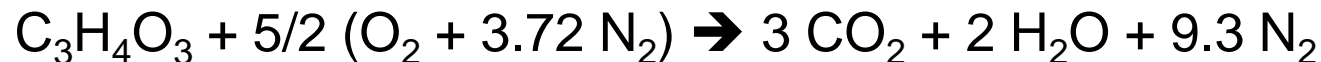
Electrolyte is composed of several chemicals

- Mixtures of
 - ethylene carbonate (EC) – $C_3H_4O_3$
 - dimethyl carbonate (DMC) – $C_3H_6O_3$
 - ethyl methyl carbonate (EMC) – $C_4H_8O_3$
 - diethyl carbonate (DEC) – $C_5H_{10}O_3$
 - ... + Lithium salt ($LiPF_6$)
- Individual mixture test at lab scale (FPA) using CDG and OC calorimetry



Definition of the chemical reaction to be used

- LP50 case : EC/EMC (1/1, wt/wt) + 12,2%wt of $LiPF_6$, neglected
- $1.14 C_3H_4O_3 + 0.96 C_4H_8O_3 + 7.16 (O_2 + 3,72 N_2) \rightarrow 7.3 CO_2 + 6.12 H_2O + 26.6 N_2$
- Average value: $\Delta H_c \approx 16$ kJ/g
- A simplified reaction used as a first approach



Then a model can be built

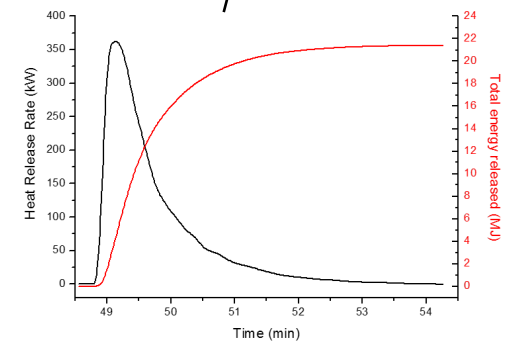
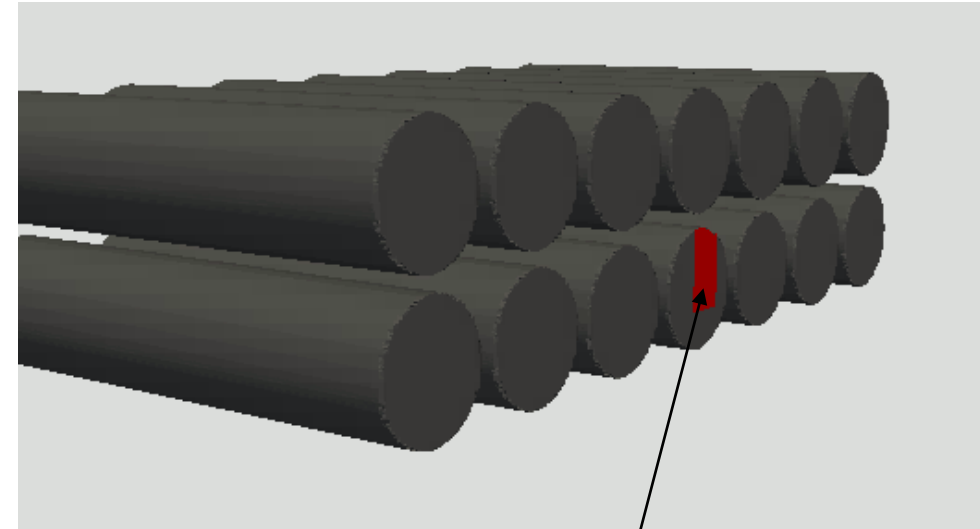
Considering the cell geometry

- **Cylinder**; Pouch; Prismatic

With a gas injection boundary condition

- Gas flow designed to reproduce the measured HRR
- Based on the chemical reaction and the ΔH_c

Considering the chemical product and reaction



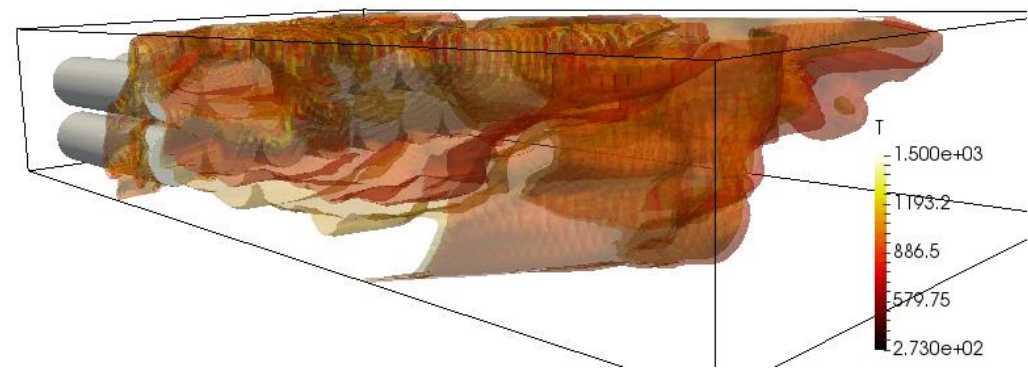
A first comparison

Fire behavior comparison in an open field, unfortunately

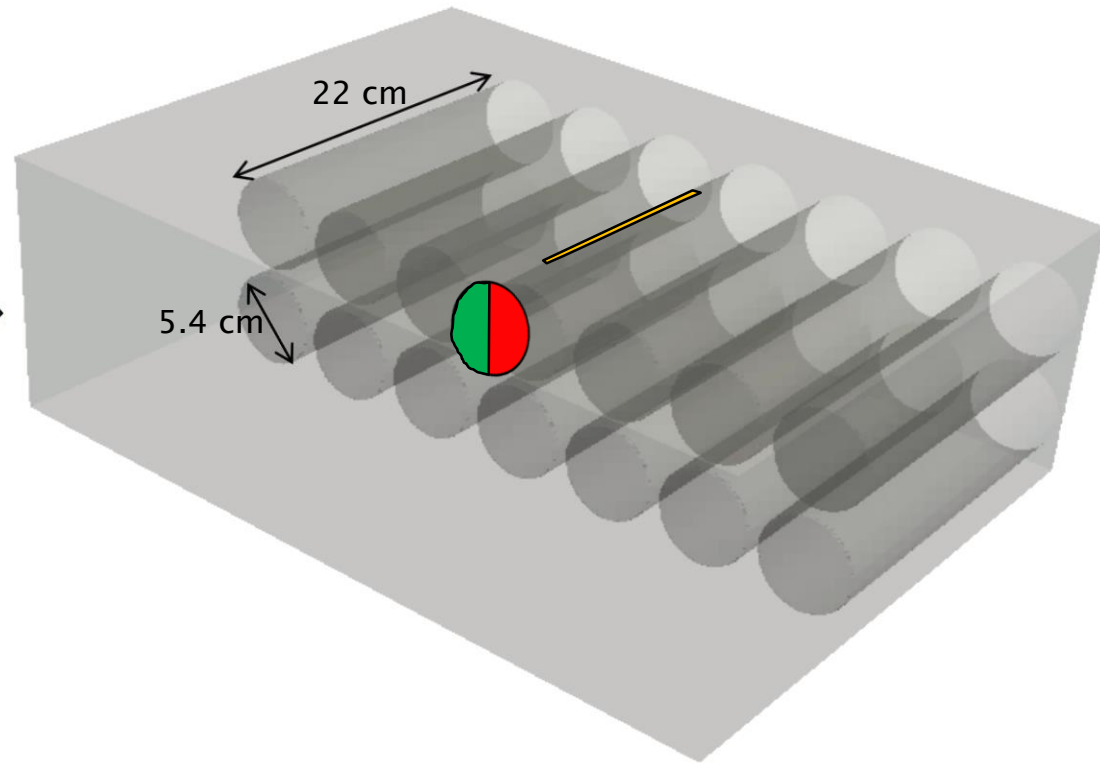
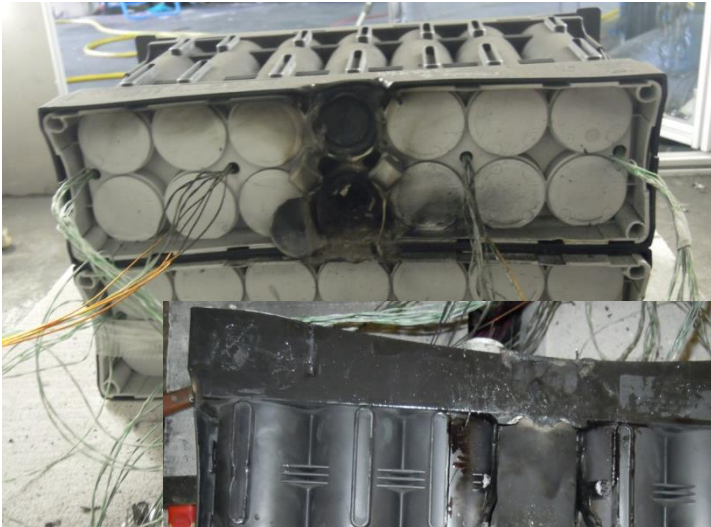
- Battery tests are not designed for CFD code validation

The flame is 3 times longer than the cell and as large as the module

- Flame length is quite correct
- Temperature is in the correct order of magnitude
- But how is representative the boundary condition?



But inside a module the flame geometry is complex



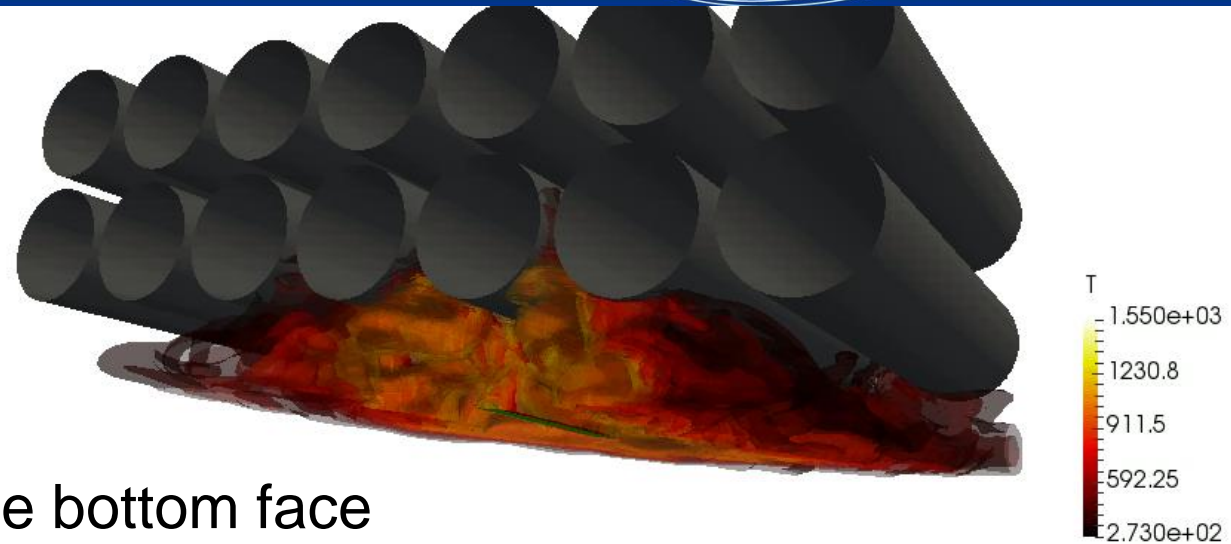
The cell opening mode is crucial

- The whole back face
- A part of the back face
- An opening along the external surface

With consequently strong fire differences

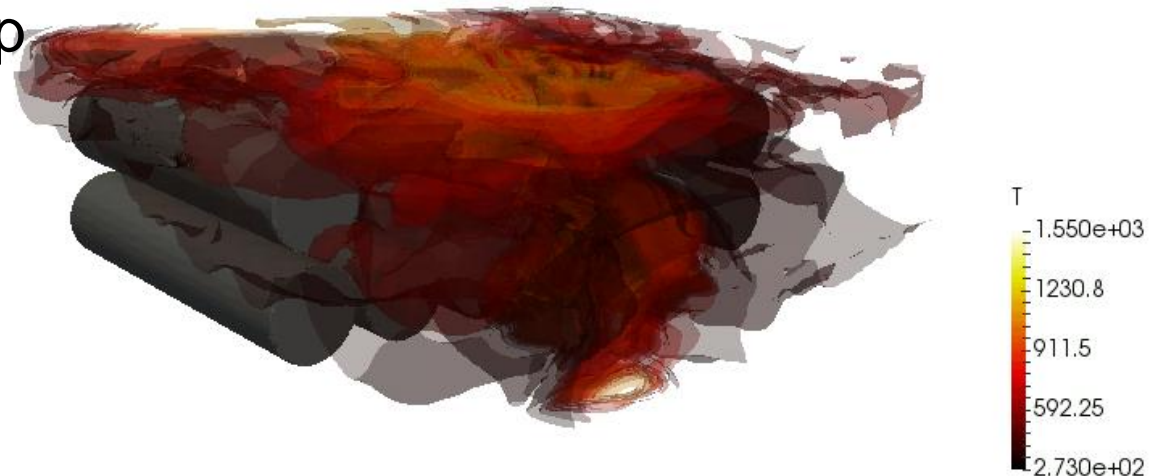
Slice for underneath cells

- Fire impinges several cells at the bottom
- Cells are mainly heated by the bottom face



Open at the back of one cell

- Fire impinges the back of the module
- Surrounding cells are heated at their back
- Some cells are heated by the top



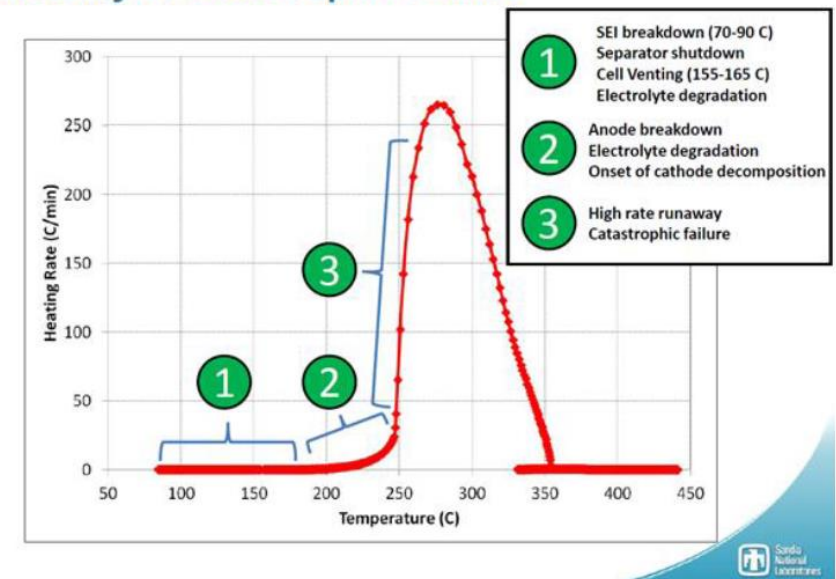
Requirement of dedicated boundary conditions

- To consider the heating of the surrounding cells
- To evaluate their ignition delay

Such an approach requires first

- To take into account the geometry of the battery
- To consider the geometry of the fire → the opening mode of the cell
- To have a correct prediction of the HRR and, consequently, of the temperature

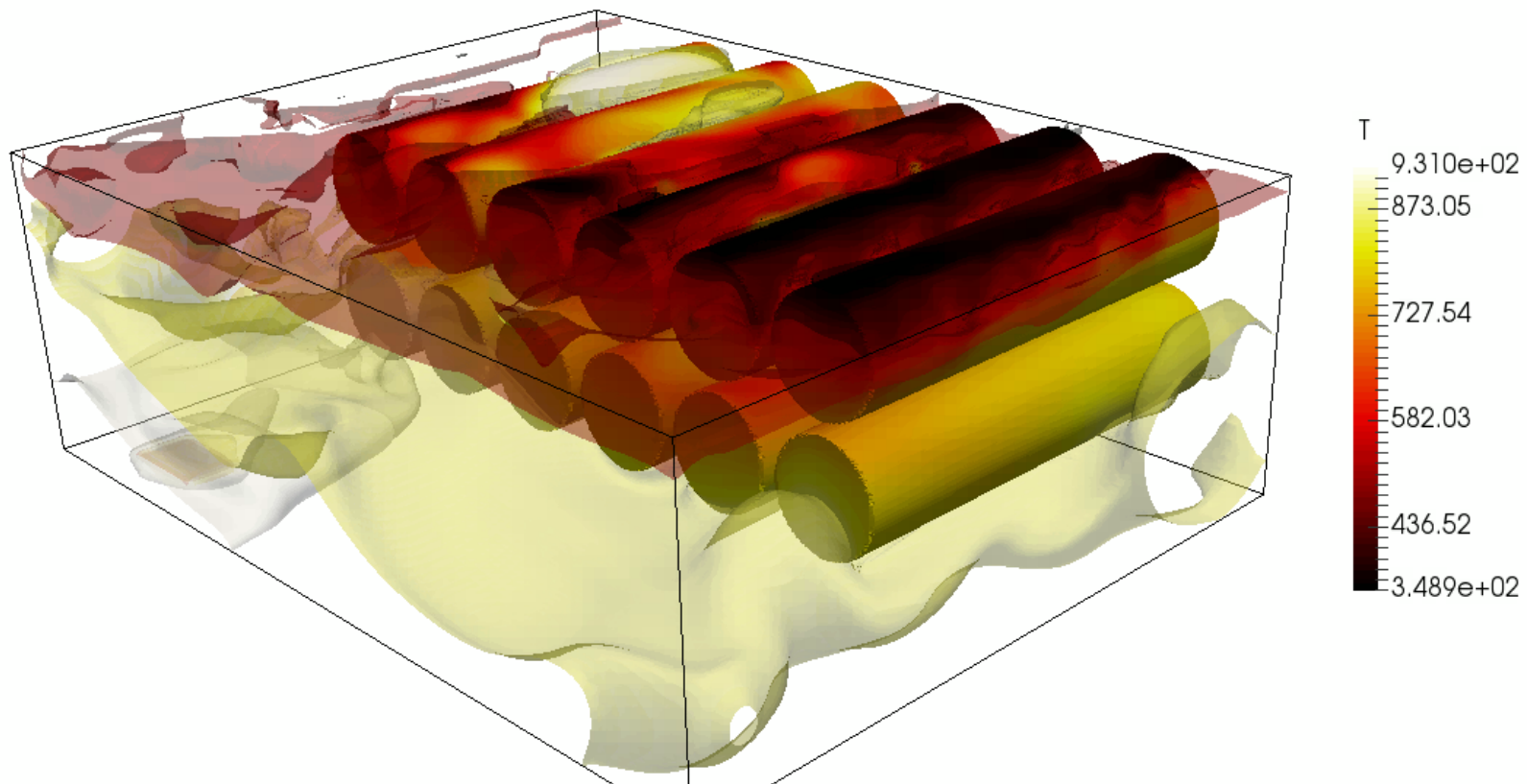
Anatomy of Catastrophic Failure



The first step: Energy given to the cell

Based on the temperature distribution

- Evolution on the cells surface along time
- Enables computation of the inner cell temperature



A very simple approach

- When the temperature reaches 155°C → cell turns into fire
- Simple to model but does not consider the specific cell volume

The considered approach

- Energy received by the cell is used to heat the electrolyte ($mC_p\Delta T$)
- When the inner cell temperature reaches 155°C → cell turns to fire
- Does not consider the electro-chemical parameters
 - To be introduced later
- Initial temperature is a critical parameter (20°C , 50°C , 80°C ?)

But non only

Cells are located into a module

Modules are placed into the LIB

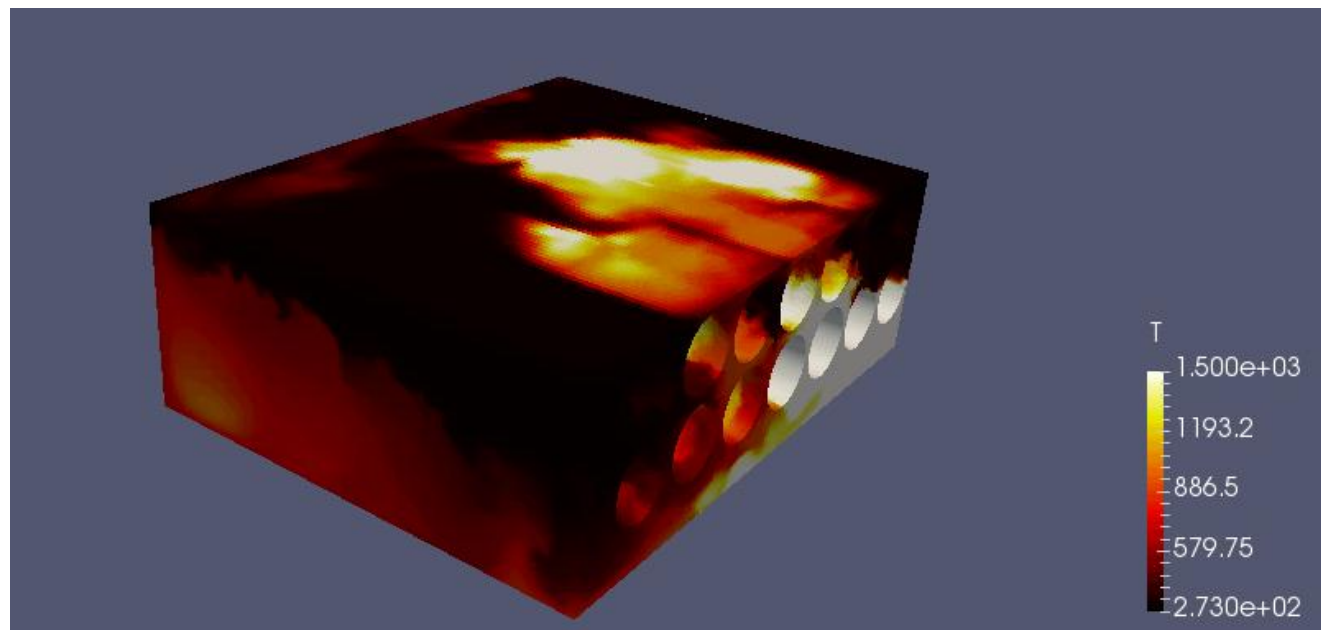
Fire ventilation is a fundamental issue

- The initial available oxygen
- The vent behavior
 - Opening based on T and P
- The cell structure breakage
 - Criteria requirement



Several steps

- Surface temperature computation
- Evaluation of the inner material temperature increase considering thermo-physical properties and thickness
- When the structure resistance reached 30% of the initial value, structure to be open (BC modification)





Achieved

- First evaluation of the FireFOAM capability
 - Geometry, chemistry, ...
- Evaluation of the input hypothesis
 - Nature of the cell opening, HRR, ...

To be done

- Confinement opening because of the temperature rise
- Module to module propagation
- Thermal protection influence evaluation

Acknowledgments

This project is receiving funding from the EU Commission under the H2020 grant agreement # 769900 under the name DEMOBASE

Coordinated by: SAFT - Name : DESPREZ Philippe

Project name : Design and Modelling for improved Battery Safety and Efficiency

- Project partners :
 - SAFT SAS
 - ACCUREC-RECYCLING GMBH
 - FRAUNHOFER GESELLSCHAFT ZUR FOERDERUNG DER ANGEWANDTEN FORSCHUNG E.V.
 - INSTITUT NATIONAL DE L'ENVIRONNEMENT ET DES RISQUES INERIS
 - INFINEON TECHNOLOGIES AG
 - MODELON AB
 - IFP Energies nouvelles
 - FORSCHUNGSZENTRUM JULICH GMBH
 - INTERACTIVE FULLY ELECTRICAL VEHICLES SRL
 - K&S GMBH PROJEKTMANAGEMENT
 - MA SPA

